## Światłowodowy interferometr pętlowy jako układ czujnikowy – przegląd możliwości aplikacyjnych

ELPROMA

IFT WAT

### Leszek R. Jaroszewicz

Instytut Fizyki Technicznej, Wojskowa Akademia Techniczna ul. gen. Sylwestra Kaliskiego 2, 00-908 Warszawa Elproma Elektronika Sp z o. o. ul. Duńska 2A, 05-152 Czosnów

20th Conference on Optical Fibers and Their Applications, Lublin 11-14.09.2023

IFT WAT

- Rys historyczny i nie tylko
- Żyroskop światłowodowy FOG jako "urealnienie" efektu Sagnaca
- Sejsmograf rotacyjny nie tak znany kuzyn FOG

ELPROMA

- System ochrony rozległych obiektów pamięci Prof. Szustakowskiego
- W pełni światłowodowy polarymetr,
- Układ lustra (reflektora) światłowodowego FLM:
  - określanie parametrów włókien,
  - pomiar współczynnika załamania ośrodka,
- Splatane fotony w służbie FOG.









ELPROMA

1904, Michelson loop interferometer (A=834 m<sup>2</sup>) for measurement the Earth rotation (1925 with z Henry G. Gale)

#### Not only historical remarks

1911 student Harress (by 1914 Herzer), measurement dispersive properties of glasses based on so called Fresnel-Fizeau drag effect.



#### [Post, Rev. Mod. Phys., 39, 1967, 475]





1911, Max von Laue "Über einen Versuch zur Optik der bewegten Körper", *Münchener Sitzungsberichte*. 405-412, describing what is today «Sagnac effect», and stating clearly that this effect can be explained classicaly or with Relativity theory.



5/22

### Sagnac effect

George Sagnac (1913)/Max Von Laue (1911) effect is a result of a difference between two optical beams propagating around closed optical path, in opposite direction when this path is rotating.

ELPROMA

The observed fringes shift is described as:

$$\Delta Z = 4\Omega . \mathbf{S} / \lambda_0 c$$

It is independent of:

- the shape of the surface S,

IFT WAT

- the location of the centre of rotation
- the presence of a rotating transparent medium

Because **massless particles** (photons) is used for the measurement, device is entirely **insensitive to linear accelerations**, **noexist cross coupling** as well as it has **BB flat response**,

 There is no moving part except photons, which allows maintenance free and small environment sensitivity





[Post, Rev. Mod. Phys., 39, 1967, 475]

The Sagnac phase shift (1976) induced by rotational rate  $\Omega$  perpendicular to plane of fiber optic sensor loop is equal to:

$$\Delta \phi = \frac{8\pi A}{\lambda c} \Omega = \frac{2\pi DL}{\lambda c} \Omega = \frac{1}{S_0} \Omega$$

where:

- A optical area
- L length of the fiber in the sensor loop

Laser

- D- sensor loop diameter
- $\lambda$  wavelength
- c velocity of the light in vacuum
- S<sub>0</sub> the optical constant of interferometer





### Fiber-Optic Gyro - FOG Fiber Optical Gyroscope



• Resonant ring of 10 to 30 cm perimeter.

**Ring Laser Gyro - RLG** 

- He-Ne plasma laser with high-voltage discharge.
- Very simple read-out signal: frequency beating.
- Dead zone about zero solved with mechanical "dither" (two 500 THz oscillators with 1 Hz difference for 1 deg/h!)
- By the way, an amusing coincidence: 400 nm and 750 nm correspond to 700 THz and 400 THz
- Improved lifetime (5 to 7 years operating) compared to mechanical gyros, but still limited: wearing-out electrodes and helium leakage

Based on lecture H. LeFavre, EWOFS-5 Kraków, 2013





- Ring interferometer with a fiber coil (100 m to 10 km over 3 to 30 cm, i.e. 0.7 to 700 m<sup>2</sup>).
- Fully solid-state components derived from optical-fiber communication components: low-attenuation single-mode optical fiber, but also, laser diode, erbium-dopedamplifying fiber, integrated optic circuit, fiber components (coupler, isolator, circulator, Bragg grating...)
- Much longer lifetime.
- Low power, low voltage.
- No acoustic noise.

1 [deg/h] ~5.10<sup>-6</sup> [rad/s] 0.01 [deg/h] for intermediate 10<sup>-8</sup> [rad/s]

	Main paremeters				
IMU Grade	ARW		SF		
	(white noise)	Bias Drift	accuracy		
	[(º/h)/√ <i>Hz</i> ]	[º/h]	[ppm]		
Rate	> 0.5	1 000 - 10	10 <sup>4</sup> -10 <sup>3</sup>		
Tactical	0.5 - 0.05	10 - 1	1 000 - 100		
Intermediate	0.05 - 0.005	1 - 0.01	100 - 1		
Inertial	0.005 - 0.0003	0.01 - 0.001	5		
Strategic	< 0.0003	< 0.001	1		













#### The baby out with the bathwater







#### **Rotational Seismometer - FOG's devil with wings**





[Kurzych et al., Opto-Elect. Rev, 28 2020) 69]

[Jaroszewicz et al., Opto-Elect. Rev, 29, 2021, 213]

10/22

04:24:10

04:24:10

FOS5-04

05:20:59.000

Aug 29, 2021

▼ max<sub>|FOS5+04|</sub> = 0.00043948 [rad/s E<sub>|FOS5-04|</sub> = 2.23e-05 [rad]

Oct 30, 2021

Oct 05, 2021

-100 1

-100



11/22



### Waveform coherency during huddle test



ELPROMA

IFT WAT

[Bernauer et al., Sensors, **21**, 2021, 264]

A high level of coherency and waveform similarity within a narrow frequency range (10 Hz - 20 Hz) for recordings from a nearby explosion signal

### IFT WAT

- ELPROMA
- Major source of phase error in FOG may occur if rapid changes in optical path length, due to thermal or mechanical effects on the fibers, because the cw and ccw beams encounter the temporally varying path length changes at different moments in time and therefore will suffer **different phase changes**!!!
- The  $d\Phi/dt$  is not readily measured directly, but by incorporating an additional optical fiber path from the source, together with the path taken by one of the counter-propagating beams from the Sagnac loop, a MZI my be formed.
- The MZI gives output proportional to  $\Phi$  and differentiation yields to required  $d\Phi/dt$ . Simple division of the Sagnac phase offset by  $d\Phi/dt$  finally gives the desired distance Z, of point of disturbance P:
- 1. rate of change  $d\Phi/dt$ , of the optical signal, induced at the point P, by external influence,
- 2. distance Z between point P and the coil centre 0



### **Perimeter security system**





#### IFT WAT **FOIPA - FO Interferometric Polarisation Analyzer** The system operation is birefringence modulation in a SMF followed by suitable detection amplitudes of first three tones Input wave SOP, DOP from output electronic signals and based on them identification polarization parameters. $(\Delta, \phi, P)$ $\Delta = \arctan(\alpha), \quad \phi = \frac{1}{2}\arctan(\beta/\gamma), \quad P = \sqrt{\beta^2 + \gamma^2}$ $\alpha = \frac{J_2(\delta_0)U2_{\omega}}{J_1(\delta_0)U2_{2\omega}}, \quad \beta = \frac{U1_{2\omega}}{2U_{01}J_2(\delta_0)}, \quad \gamma = \frac{1}{2U_{02}} \sqrt{\left(\frac{U2_{\omega}}{J_1(\delta_0)}\right)^2 + \left(\frac{U2_{2\omega}}{J_2(\delta_0)}\right)^2}$

The system require fulfillment IV-th Fresnel-Argo interference condition (interaction of two orthonormal polarized beams).





15/22

 $f(t) = \delta \cos \omega t$ 





ELPROMA

[Jaroszewicz et al., *IEEE Sensor J.*, **3**, 2003]



16/22



-60

-65

1544

1546

 $\lambda_1$ 

1548

 $\lambda_2$ 

1554

1556

1558

λ

1550

λ (nm)

1552

$$\frac{d\Delta\varphi}{dX} = \frac{2\pi}{\lambda} \left( L \frac{\partial\Delta n}{\partial X} dX + \Delta n \frac{\partial L}{\partial X} dX \right)$$



Światłowód

Światłowód

# 

#### **Phase & group birefringence**





#### **Modal birefringence sensitivity**





#### **Refractive index measurement**



[Zawisza et al., Sensors, 18, 2018, 2370]

IFT WAT

Fiber coil

SIAPD

Source

Wi-Fi antenna

PC



detection

interferometer

#### **Entanglement- enhanced optical gyro**





[Fink et al., New J. Phys., 21, 2019, 053010]

laser diode

HWP

ppKTP

YVO4

Lens

source

PMF

dichroic mirror

mirror

two-photon state  $|\Psi^{PMF}\rangle$ 

**Table 2.** Comparison of the measurement precision with M = 1955 photons detected on average. Standard quantum limit  $\Delta \Omega^{\text{SNL}} = 1/(S\sqrt{M})$  and Heisenberg limit  $\Delta \Omega^{\text{HL}} = 1/(SM)$  of the measurement system, with the scale factor S = 1.09. Best precision of the respective measurement run  $\Delta \Omega_{\min}$  (blue colored data in figure 4). Precision at the bias point  $\Delta \Omega_{\text{Bias}}^{\text{E}}$ , estimated via fit function. All values are given in rad s<sup>-1</sup>.

Ν	$\Delta\Omega^{\rm SNL}$		$\Delta\Omega_{\rm min}$	$\Delta\Omega^{\rm E}_{\rm Bias}$		$\Delta\Omega^{\rm HL}$
1 2	0.0207	≯ >	0.025(0) 0.018(9)	0.024 8 0.018 3	> >	$469 \times 10^{-6}$

- Ω [rad s<sup>-1</sup>]

2π



### Thank you for your attention

### this work has been made under financial suport National Center for Research and Development, Poland project – POIR.01.01.01-00-1553/20-00

